Detailed Studies of **Electron Cooling Friction Force**

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(September 30, 2005)





Outline

Part 1:

Numerical studies and comparison with theory.

A. Fedotov, D. Bruhwiler, D. Abell, A. Sidorin, "Detailed studies of the friction force", COOL05 Workshop (Galena, IL)

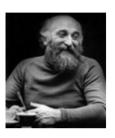
Part 2:

Experimental studies of the friction force.

A. Fedotov, B. Galnander, V. Litvinenko, T. Lofnes, A. Sidorin, A. Smirnov, V. Ziemann, "Experimental benchmarking of the magnetized friction force", COOL05 Workshop (Galena, IL)







Electron cooling was invented by G.I. Budker (INP, Novosibirsk, 1966)

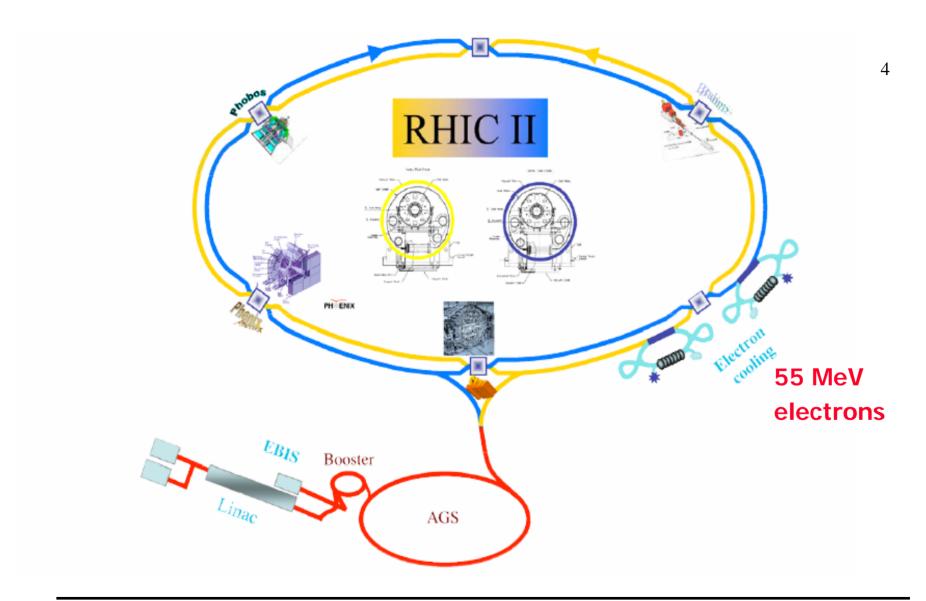


First experimental cooling. NAP-M storage ring (Novosibirsk, 1974)

- 1. Low-energy (3-300 KeV electrons) cooling (1974-2005): 10's of coolers were constructed and successfully operated all based on magnetized cooling.
- 2. Medium-energy (4 MeV) cooling at FNAL: first non-magnetized cooling demonstrated July 2005.
- 3. Future medium and high-energy cooling projects: HESR (GSI) and RHIC-II (BNL).











Practical implementation of e-cooling

- 1. Produce a beam of cold (low emittance) electrons.
- 2. Move these electrons with a velocity of the heavy particles to be cooled.
- 3. Heavy particles scatter off the electrons and energy is transferred to electrons. This energy transfer appears as a friction force acting on the ions. The ions are "cooled".
- 4. The electrons are renewed.





Physics of magnetized and non-magnetized cooling

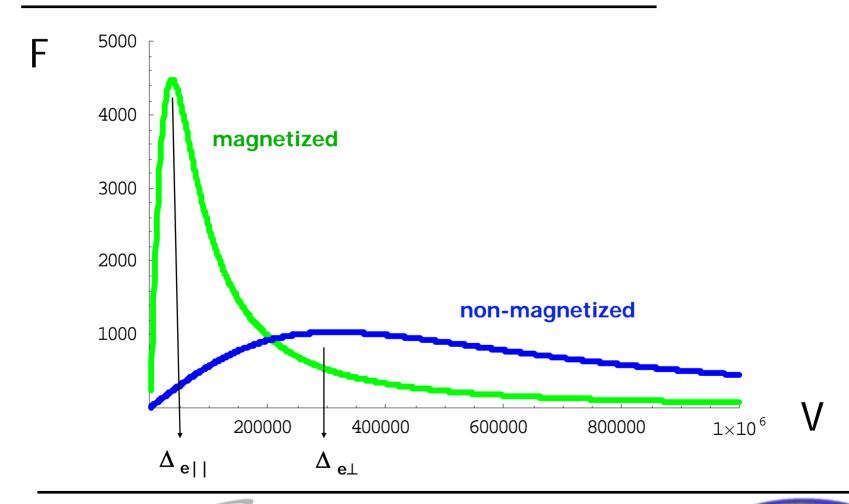
- 1. Non-magnetized cooling: thermal velocity of electrons smaller than the velocity spread of ions which needs to be cooled.
- 2. Magnetized cooling: strong magnetic field limits transverse motion of electrons, so that transverse degree of freedom does not take part in the energy exchange. As a result, the efficiency of cooling is determined only by the longitudinal velocity spread of electrons.

In typical low-energy coolers longitudinal velocity spread of electrons is much smaller than transverse – strong velocity anisotropy together with magnetic field leads to "fast cooling".





Schematic friction force for magnetized and nonmagnetized cooling







Future high-energy coolers

- 1. HESR (GSI) cooler up to 8MeV electrons. Present baseline 4MeV as in FNAL. However, it needs to be magnetized cooling many technical issues.
- 2. RHIC-II (BNL)- cooling with bunched electron beam with energy up to 55MeV first high-energy cooling based on new technology.





Limitation of magnetized cooling at high-energy

A problem of Magnetized Cooling for high-energy is that "effective longitudinal spread of electron" due to magnetic imperfection can be rather big:

1. RHIC (BNL): γ =100, θ =1e-5, θ _ effective= $\gamma\theta$ =1e-3

To get significant advantage from "good Magnetized Cooling" – one needs to make precise solenoid (or have a scheme of precise alignment). The main purpose of magnetized cooling approach for RHIC is to kill recombination.

2. HESR (GSI): γ =9, θ =1e-5, θ _effective=9e-5

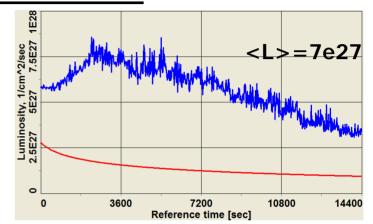




RHIC e-cooling

For electron cooling in RHIC (Au ions at γ =108) we studied two approaches:

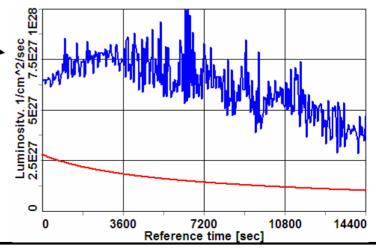
1. Magnetized cooling – B=2-5T \sim solenoid, L=2x30m, q=20nC, ϵ_e =50 um



Factor of 10 increase in luminosity in both approaches

2. Non-magnetized cooling (with helical wigglers to control recombination) – B=20-50G, L=2x30m, q=2-5nC, ε_e=2-3um

RHIC E-cooler Design Report http://www.agsrhichome.bnl.gov/eCool







High-energy cooling: need for accurate predictions of cooling times

Cooling times for relativistic energies are much longer than for typical coolers:

$$\tau = \frac{A}{Z^2} \frac{\gamma^2}{4\pi r_p r_e n_e c \, \eta \Lambda_c} \left(\frac{\gamma \varepsilon_{in}}{\beta_{ic}}\right)^{3/2}$$

- standard (order of magnitude) estimate of cooling times for Au ion at RHIC storage energy of 100 GeV gives τ of the order of 1000 sec, compared to a typical cooling time of the order of 0.1-1 sec in existing coolers
- while an order of magnitude estimate was sufficient for typical coolers it becomes unacceptable for RHIC with a store time of a few hours and fast emittance degradation due to Intra Beam Scattering (IBS)

We need computer simulations which will give us cooling times estimates with an accuracy much better than an order of magnitude.





Accurate description of the Cooling Force



- 1. Benchmarking of available formulas vs VORPAL code (direct simulation of friction force) for various regimes.
- D. Bruhwiler et al., AIP Conf. Proc. 773 (Bensheim, Germany, 2004), p.394.
- A. Fedotov et al.; Bruhwiler et al., Proceedings of PAC'05 (Knoxville, TN, 2005).
- 2. Experimental benchmarking:

(CELSIUS, December 2004 and March 2005)





Part 1

(Friction force formulas: theory and simulations)

A. Fedotov (BNL), D. Bruhwiler, D. Abell (Tech-X), A. Sidorin (JINR)





Comparison with theory

At a minimum, we want to be sure that we are using the most appropriate and accurate cooling force formulas.

Magnetized friction force:

"electron cooling theory is well understood"

- 1. Infinite magnetic field appoximation (Derbenev-Skrinsky (D-S), Derbenev-Skrinsky-Meshkov (D-S-M)).
- 2. Empiric formula (V. Parkhomchuk (VP)) (any strength of the field) can show very different cooling dynamics for some parameters. Also, has different numerical factors.

Different formulas agree with one another within factor of 3-10, depending on the parameters – not good for high-energy estimates.

Non-magnetized force:

More straightforward – but one needs to use correct expressions - we did comparison of typically used asymptotic formulas and direct numerical integration.





Codes used for Friction Force studies

We use:

- 1. VORPAL code uses molecular dynamics techniques to explicitly resolve close binary collisions and thus capture friction and diffusion tensors with a bare minimum of physical assumptions.
 - C. Nieter, J. Cary, J. Comp. Phys. 196, p. 448 (2004)
 - D. Bruhwiler et al., AIP Conf. Proc. 773 (Bensheim, 2004), p. 394.
- 2. Numerical integration of analytic formulas over electron velocity distribution and comparison with simple asymptotic expressions using BETACOOL code

The BETACOOL program, http://lepta.jinr.ru





Non-magnetized friction force (B=0) – isotropic electron distribution

$$\vec{F} = -\frac{4\pi n_e e^4 Z^2 L}{m} \int \frac{\vec{v}_i - \vec{v}_e}{\left|\vec{v}_i - \vec{v}_e\right|^3} f(v_e) d^3 v_e$$

For isotropic Maxwellian distribution $f(v_e)$ (Chandrasekar 1942):

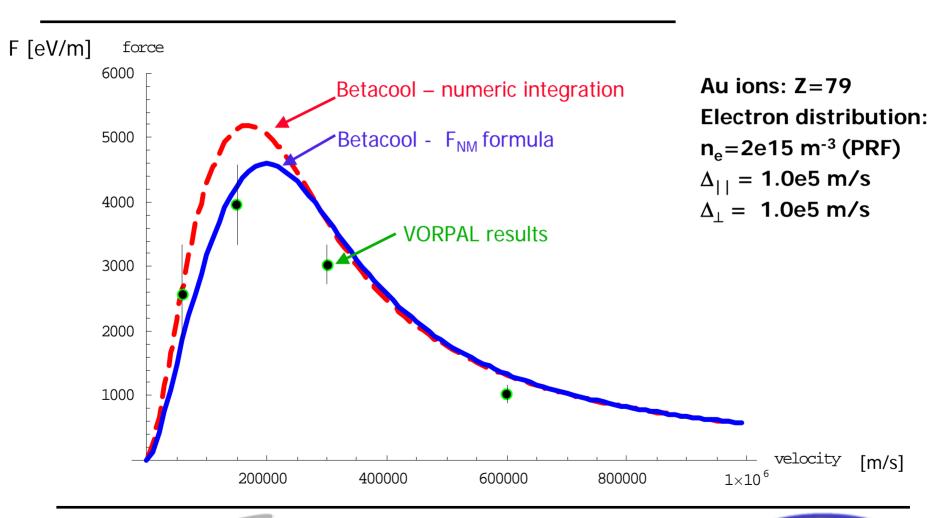
$$\vec{F}_{NM}(\vec{v}_i) = -\frac{\vec{v}_i}{v_i^3} \frac{4\pi n_e e^4 Z^2 L}{m} \varphi \left(\frac{v_i}{\Delta_e}\right)$$

$$\varphi(x) = \sqrt{\frac{2}{\pi}} \int_{0}^{x} e^{-y^{2}/2} dy - \sqrt{\frac{2}{\pi}} x e^{-x^{2}/2}$$





B=0, isotropic electron distribution for ion velocity along the longitudinal direction







B=0 – anisotropic electron velocity distribution (typical situation for electron coolers)

Numerical evaluation (BETACOOL):

$$F_{\perp} = -\frac{4\pi Z^{2}e^{4}n_{e}}{m \cdot Int} \int_{0}^{3\Delta_{\parallel}} \int_{-3\Delta_{\parallel}}^{3\Delta_{\parallel}} \int_{0}^{\pi} \ln\left(\frac{\rho_{\text{max}}}{\rho_{\text{min}}}\right) \frac{\left(V_{\perp} - v_{\perp}\cos\varphi\right) \exp\left(-\frac{v_{\perp}^{2}}{2\Delta_{\perp}^{2}} - \frac{v_{\parallel}^{2}}{2\Delta_{\parallel}^{2}}\right)}{\left(\left(V_{\parallel} - v_{\parallel}\right)^{2} + \left(V_{\perp} - v_{\perp}\cos\varphi\right)^{2} + v_{\perp}^{2}\sin^{2}\varphi\right)^{3/2}} v_{\perp}d\varphi dv_{\parallel}dv_{\perp}$$

$$F_{\parallel} = -\frac{4\pi Z^{2}e^{4}n_{e}}{m \cdot Int} \int_{0}^{3\Delta_{\perp}} \int_{-3\Delta_{\parallel}}^{3\Delta_{\parallel}} \int_{0}^{\pi} \ln\left(\frac{\rho_{\text{max}}}{\rho_{\text{min}}}\right) \frac{\left(V_{\parallel} - v_{\parallel}\right) \exp\left(-\frac{v_{\perp}^{2}}{2\Delta_{\perp}^{2}} - \frac{v_{\parallel}^{2}}{2\Delta_{\parallel}^{2}}\right)}{\left(\left(V_{\parallel} - v_{\parallel}\right)^{2} + \left(V_{\perp} - v_{\perp}\cos\varphi\right)^{2} + v_{\perp}^{2}\sin^{2}\varphi\right)^{3/2}} v_{\perp} d\varphi dv_{\parallel} dv_{\perp}$$

Asymptotic formulas – can significantly overestimate friction force, especially near the longitudinal rms velocity spread

$$(\Delta_{\parallel} << V_{j} << \Delta_{\perp})$$

$$F_{\parallel} = -\frac{4\pi Z^{2} e^{4} n_{e} L}{m} \frac{V_{\parallel}}{\Delta_{\parallel} \Delta_{\perp}^{2}}$$

$$\vec{F}_{\perp} = -\frac{4\pi Z^{2} e^{4} n_{e} L}{m} \frac{V_{\parallel}}{\Delta_{\perp}^{2}}$$

$$\vec{F}_{\parallel} = -\frac{4\pi Z^{2} e^{4} n_{e} L}{m} \frac{V_{\parallel}}{V_{\parallel} |\Delta_{\perp}^{2}}$$

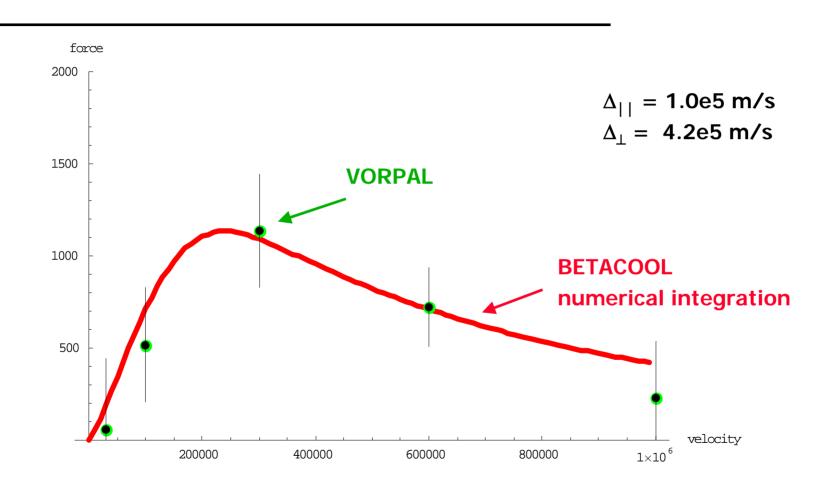
$$\vec{F}_{\parallel} = -\frac{4\pi Z^{2} e^{4} n_{e} L}{m} \frac{V_{\parallel}}{V_{\parallel} |\Delta_{\perp}^{2}}$$

$$\vec{F}_{\parallel} = -\frac{4\pi Z^{2} e^{4} n_{e} L}{m} \frac{V_{\parallel}}{V_{\parallel} |\Delta_{\perp}^{2}}$$





B=0, anisotropic velocity distribution







Non-magnetized force - summary

For anisotropic velocity distribution:

- 1. VORPAL gives good agreement with numerical integrals.
- 2. Asymptotic formulas overestimate friction force by a significant factor for typical RHIC parameters.

We are presently using numerical integrals in BETACOOL in our cooling dynamics studies for the non-magnetized cooling.





Magnetized friction force

- approximation of strong magnetic field

Numerical integration using Derbenev-Skrinsky (D-S) expressions for the magnetized collisions (BETACOOL):

$$\begin{split} F_{\perp} \left(V_{\perp}, V_{\parallel} \right) &= -\frac{2\pi Z^{2} e^{4} n_{e} L_{M}}{m} \int \frac{V_{\perp} \left(V_{\perp}^{2} - 2 \left(V_{\parallel} - v_{e} \right)^{2} \right)}{\left(V_{\perp}^{2} + \left(V_{\parallel} - v_{e} \right)^{2} \right)^{5/2}} f\left(v_{e} \right) dv_{e} \\ F_{\parallel} \left(V_{\perp}, V_{\parallel} \right) &= -\frac{2\pi Z^{2} e^{4} n_{e}}{m} \int \left(L_{M} \frac{3V_{\perp}^{2} \left(V_{\parallel} - v_{e} \right)}{\left(V_{\perp}^{2} + \left(V_{\parallel} - v_{e} \right)^{2} \right)^{5/2}} + 2 \frac{V_{\parallel} - v_{e}}{\left(V_{\perp}^{2} + \left(V_{\parallel} - v_{e} \right)^{2} \right)^{3/2}} \right) f\left(v_{e} \right) dv_{e} \end{split}$$

Asymptotic expressions for all three type of collisions

(Derbenev-Skrinsky-Meshkov (D-S-M)):

$$F_{\perp} \approx -\frac{2\pi Z^{2}e^{4}n_{e}}{m}v_{\perp} \begin{cases} \frac{1}{v^{3}} \left(2L_{F} + \frac{v_{\perp}^{2} - 2v_{\parallel}^{2}}{v^{2}}L_{M}\right), \{I\} \\ \frac{2}{\Delta_{\perp}^{3}} \left(L_{F} + N_{col}L_{A}\right) + \frac{v_{\perp}^{2} - 2v_{\parallel}^{2}}{v^{2}} \frac{L_{M}}{v^{3}}, \{II\} \end{cases} F_{\parallel} \approx -\frac{2\pi Z^{2}e^{4}n_{e}}{m}v_{\parallel} \begin{cases} \frac{1}{v^{3}} \left(2L_{F} + \frac{3v_{\perp}^{2}}{v^{2}}L_{M} + 2\right), \{I\} \\ \frac{2}{\Delta_{\perp}^{2}v_{\parallel}} \left(L_{F} + N_{col}L_{A}\right) + \left(\frac{3v_{\perp}^{2}}{v^{2}}L_{M} + 2\right) \frac{1}{v^{3}}, \{II_{a}\} \\ \frac{2}{\Delta_{\perp}^{2}} \left(L_{F} + N_{col}L_{A}\right) + \frac{L_{M}}{\Delta_{\parallel}^{3}}, \{III\} \end{cases}$$





Finite magnetic field

Empiric formula by V. Parkhomchuk (VP) (NIM, 2000):

$$\vec{F} = -\vec{v} \frac{4Z^2 e^4 n_e L_P}{m} \frac{1}{\left(v^2 + \Delta_{e,eff}^2\right)^{3/2}} \qquad L_P = \ln\left(\frac{\rho_{\text{max}} + \rho_{\text{min}} + \langle \rho_{\perp} \rangle}{\rho_{\text{min}} + \langle \rho_{\perp} \rangle}\right)$$

- 1. Similar to D-S asymptotics at low velocities $v < \Delta_{||}$
- 2. Very different at large velocities $v >> \Delta_{||}$ both in numerical factor and dependence on angle with respect to the magnetic field direction.

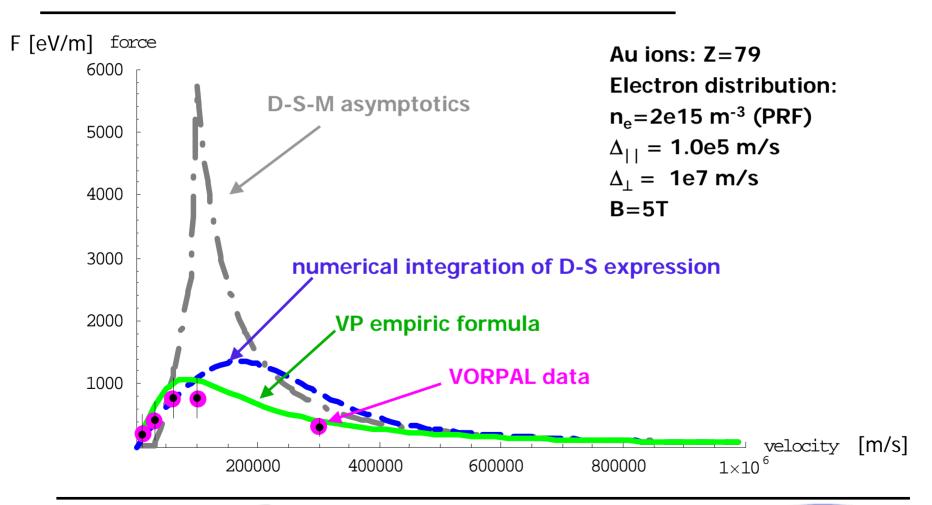
Studies were done to explore magnetized friction force formulas in various regimes. Some of these studies are reported in the next few slides, using parameters of the RHIC-II cooler based on the magnetized approach.





Friction force for ion velocity along magnetic field line

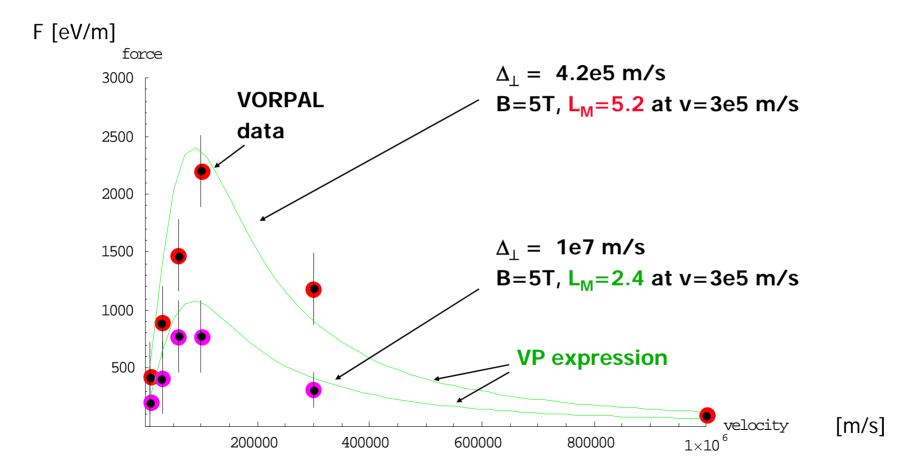
 $\mathbf{V}_{\perp} = \mathbf{0}$ 23







Friction force for ion velocity along magnetic field line $(V_{\perp} = 0)$ for two different degrees of magnetization







Angular dependence at large relative velocities

Strong magnetic field results in friction force dependence on the angle with respect to the direction of magnetic field.

Very different expressions for the transverse and longitudinal components of the friction force both of which now depend on both transverse and longitudinal velocity.

But how important is such "angular anisotropy" of the friction force for finite magnetization?

This question was already addressed by Parkhomchuk (NIM, 2000), using simulations with zero temperature electrons. Here we try to examine this question for finite temperatures of electron beam.





Angular dependence for longitudinal component of the friction force

empiric formula by V. Parkhomchuk (VP)

$$\mathbf{F}^{VP} = -\frac{1}{\pi} \omega_{pe}^2 \frac{(Ze)^2}{4\pi\varepsilon_0} \Lambda^M \frac{\mathbf{V}_{ion}}{(V_{ion}^2 + V_{eff}^2)^{3/2}}$$

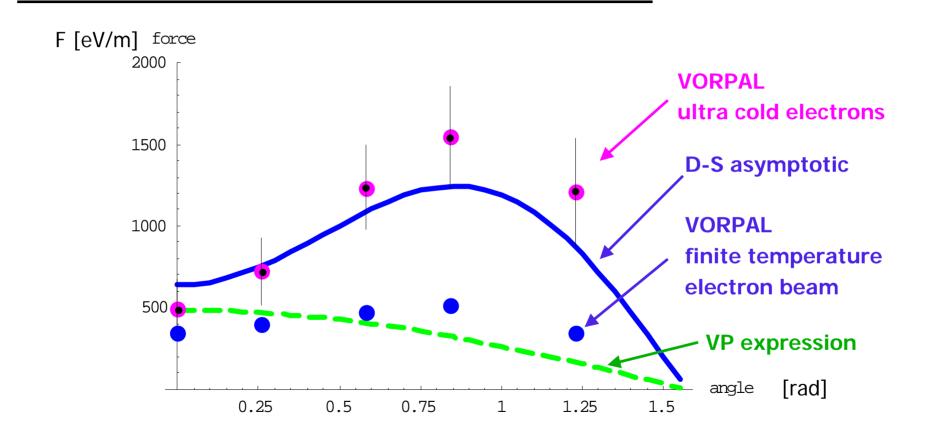
Derbenev-Skrinsky (D-S) asymptotic

$$\mathbf{F}_{\parallel}^{DS} = -\frac{3}{2}\omega_{pe}^{2} \frac{(Ze)^{2}}{4\pi\varepsilon_{0}} \left[\Lambda^{A}(V_{ion}) \left(\frac{V_{\perp}}{V_{ion}} \right)^{2} + \frac{2}{3} \right] \frac{V_{\parallel}}{V_{ion}^{3}}$$





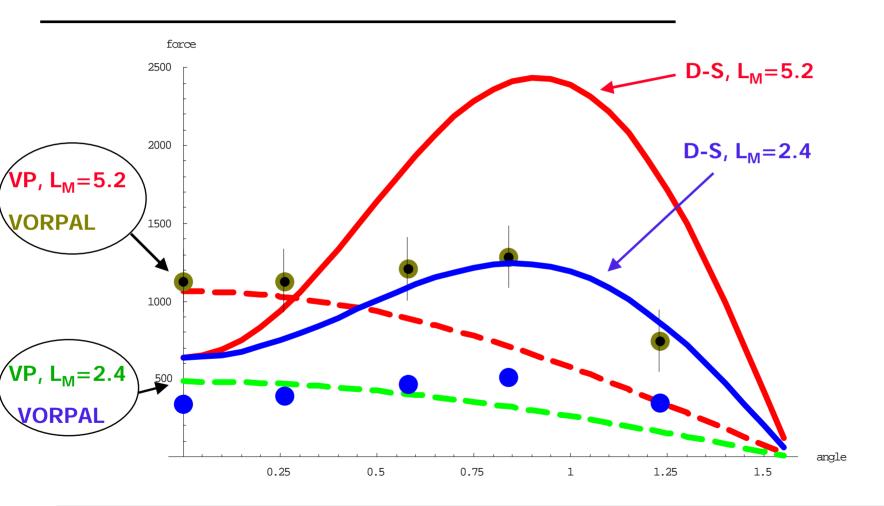
Angular dependence for Vion=3e5 m/s (B=5T, for $\Delta_{\rm ex,y}$ =8e6 m/s, $L_{\rm M}$ =2.4)







Longitudinal friction force – scaling with magnetized logarithm for finite temperature electron beam







Transverse component of friction force for high velocities $V > \Delta_{e\parallel}$

$$D-S_{d} (1977)$$

$$F_{\perp,dialectric}^{DS} = -\frac{1}{2} \omega_{pe}^{2} \frac{(Ze)^{2}}{4\pi\varepsilon_{0}} \Lambda^{A}(V_{ion}) \frac{(V_{\perp}^{2} - 2V_{\parallel}^{2})}{V_{ion}^{2}} \frac{V_{\perp}}{V_{ion}^{3}}$$

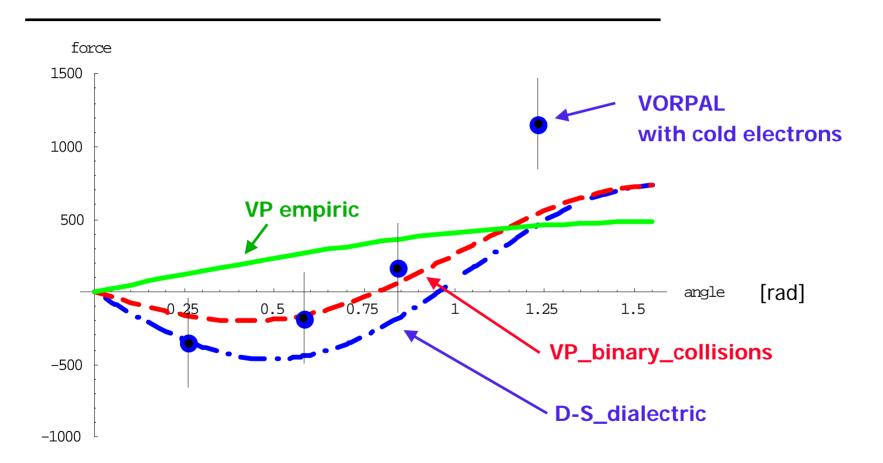
$$P_{\text{binary collisions}} (1984)$$

$$F_{\perp,binary}^{P} = -\frac{1}{2} \omega_{pe}^{2} \frac{(Ze)^{2}}{4\pi\varepsilon_{0}} \Lambda^{A}(V_{ion}) \frac{(V_{\perp}^{2} - V_{\parallel}^{2})}{V_{ion}^{2}} \frac{V_{\perp}}{V_{ion}^{3}}$$





Angular dependence for the transverse component of the friction force







Conclusions on magnetized formulas

Using VORPAL code we are now able to explore fine effects in magnetized cooling.

We are studying accuracy of available formulas and theories in various regimes.





Part 2

(Experimental benchmarking of the friction force)

- A. Fedotov, V. Litvinenko (BNL)
- B. Galnander, T. Lofnes, V. Ziemann (TSL)
- A. Sidorin, A. Smirnov (JINR)





Svedberg Laboratory, Uppsala, Sweden (The CELSIUS ring)

Team:

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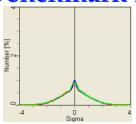


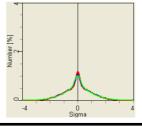


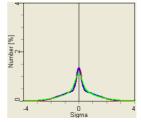


Major goals

- 1. With well controlled experiments systematically study friction force dependence on various parameters such as current, alignment angle, magnetic field.
- 2. Using low-energy cooler try to reproduce conditions possible at high-energy cooling:
- 2.1) Different magnetization regimes possible transition from good to bad magnetization
- 2.2) Transient cooling when as a result of slow cooling one first has clear formation of beam core with subsequent cooling of tails need to benchmark IBS models for such distributions. very important







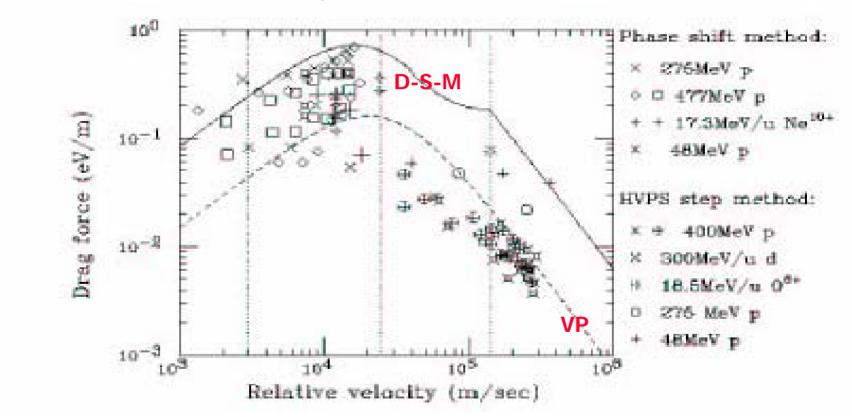
for collider





Example of some previous comparison of experimental data with Derbenev-Skrinsky-Meshkov (D-S-M) and V.Parkhomchuk (VP) formulas.

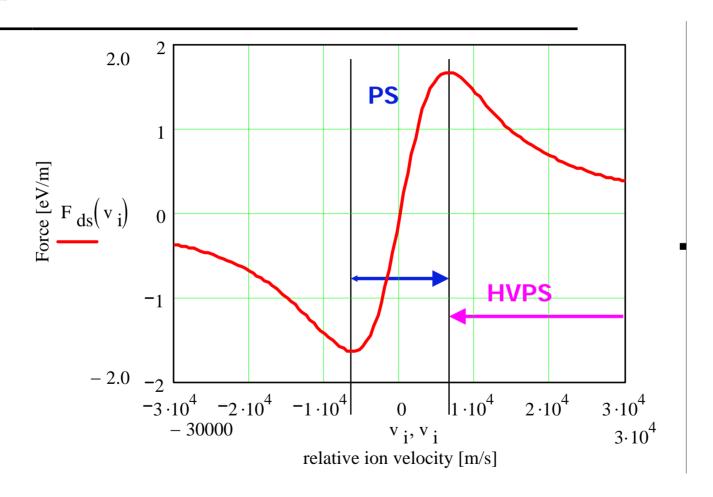
Y-N. Rao et al.: CELSIUS, Sweden'2001:







Measurement methods: Phase Shift (PS) and Voltage Step (HVPS)







Low relative velocities (linear part and maximum): Phase shift (PS) method

• The phase shift method is to apply both the electron cooling and the rf system (bunched ion beam):

measure the phase shift at equilibrium where the energy gain that an ion beam receives on passage through the rf cavity is equal to the energy loss during passage through the cooler

$$F_{\parallel} = \frac{Ze\hat{U}_{rf}\sin\Delta\phi_{s}}{L_{c}}$$

U_{rf} –the rf amplitude

 $\Delta\phi_s$ –the equilbrium phase difference between the bunch and rf cavity

L_c - length of the cooler





Large relative velocities: HVPS method

• The electron beam energy is stepped by quickly changing the HVPS voltage:

The electron beam begins to drag the ion beam as a whole to a new energy corresponding to the new energy of electron beam. During this process the ion beam energy is tracked by recording its Schottky frequency shift

$$F_{\parallel} = \frac{1}{\eta_p} \frac{p_0}{f_0} \frac{\Delta f}{\Delta t} \cdot \frac{1}{\eta_{ec}}$$

 η_p — slippage factor, p_0 is ion momentum

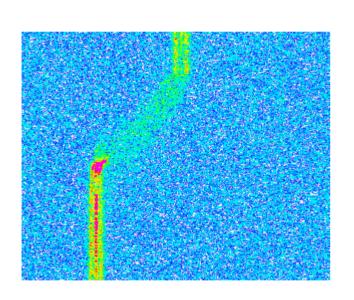
 $\eta_{\rm ec}$ – L/C – ration of cooler length to circumference

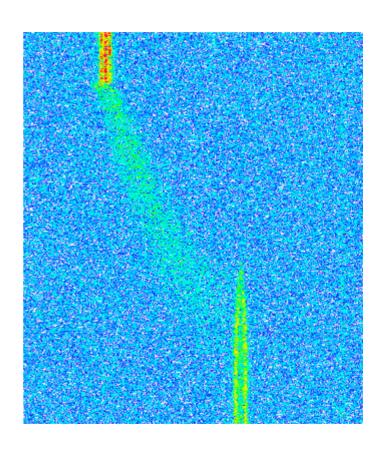
 Δf – frequency shift recoded during time Δt





Accuracy of HVPS method









- 1. One needs to introduce small velocity difference between electrons and ions typically, voltage step is used to change energy of electrons.
- 2. One needs accurate measurement of the phase difference between the bunch and RF signal.

In our experiment at CELSIUS:

- 1. Changing RF frequency allowed very fine steps in velocity difference (done before, for example, at IUCF).
- 2. Instead of network analyzer without phase lock loop the phase was measured by phase discriminator.

As a result, very accurate experimental data was obtained!





Experiment #1:

1. B=0.1T, current dependence: (Ie=500mA, 250mA, 100mA, 20 mA)

Measure all needed parameters, including parameters of ion distribution.





Experiment #2:

2. Dependence on **V**_effective:

- measured for several values of tilt in both horizontal and vertical direction both negative and positive directions.
- always recorded longitudinal and transverse sigmas to perform accurate convolution over distributions. Measured values are close to those predicted by BetaCool simulations
- did calibration of tilt angle with both BPM's and H⁰ monitor

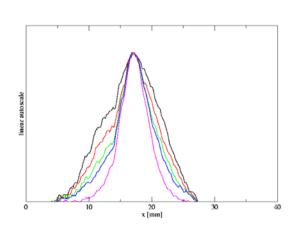


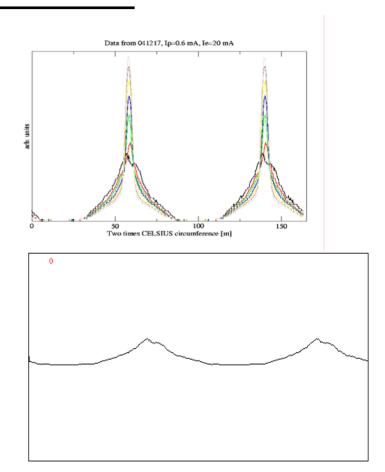


Experiment #3:

3. Measured "transient cooling" (IBS+COOLING) both for longitudinal and transverse profiles:

Test models of IBS for non-Gaussian distribution -needed for high-energy cooling.









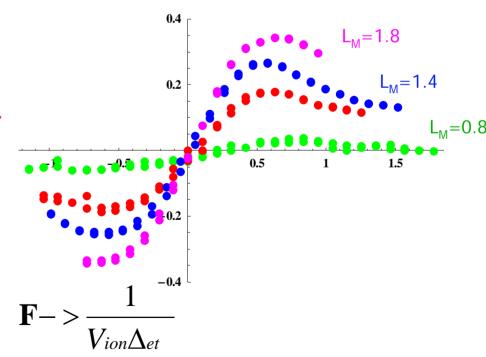
Experiment #4:

4. Various values of B with various currents: Ie=500mA, 300mA, 100mA, 50 mA (B=0.03, 0.04, 0.05, 0.06, 0.08, 0.1, 0.12T) - a lot of careful adjustments for each new setting of magnetic field.

Study various regimes of magnetization – needed for high-energy cooling.

$$L_M = \ln\left(\frac{\rho_{\text{max}}}{r_L} + 1\right) = \frac{\rho_{\text{max}}}{r_L}$$

$$\mathbf{F} = -\frac{1}{\pi} \omega_{pe}^2 \frac{(Ze)^2}{4\pi\varepsilon_0} \frac{1}{(V_{ion}^2)} (V\tau eB/m\Delta_{et}) \qquad \mathbf{F} -$$







Experiment #5:

5. Effects of solenoid errors.

Study description via V_effective.





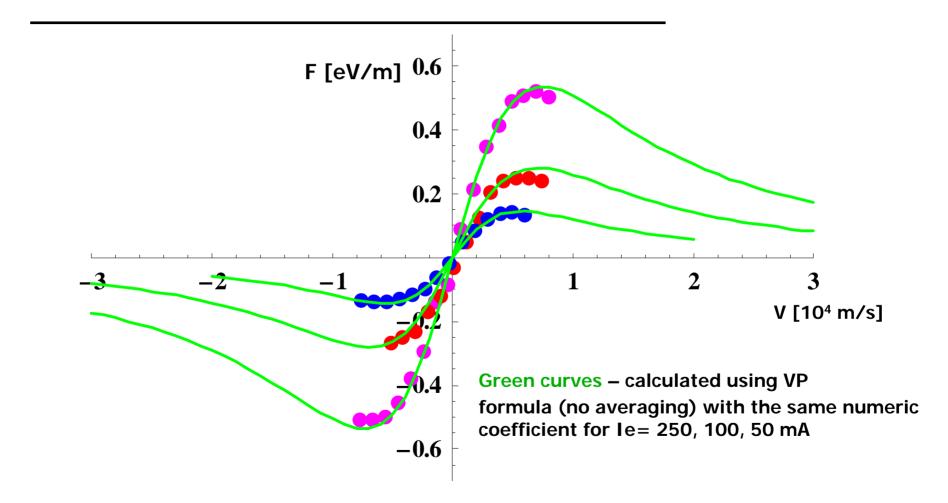
V. Parkhomchuk's (VP) empiric formula

empiric formula (VP) - single-particle formula

$$\mathbf{F} = -\frac{1}{\pi} \omega_{pe}^2 \frac{(Ze)^2}{4\pi\varepsilon_0} \ln \left(\frac{\rho_{\text{max}} + \rho_{\text{min}} + r_L}{\rho_{\text{min}} + r_L} \right) \frac{\mathbf{V}_{ion}}{(V_{ion}^2 + V_{eff}^2)^{3/2}}$$





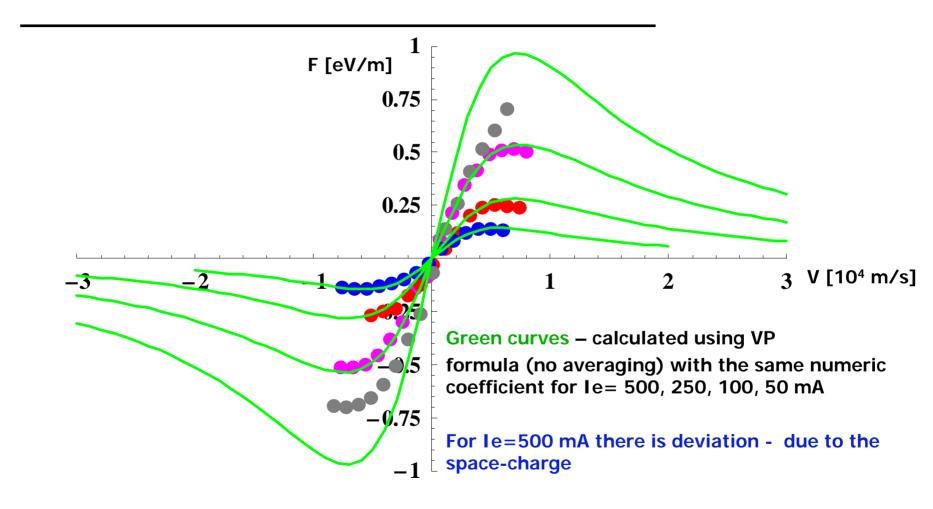






Ie=500 (gray), 250 (pink), 100 (red), 50 (blue) mA

48







Electron current Ie=500mA

For high currents of the electron beam the space-charge of the electron beam becomes important:

The electron drift in crossed fields – the electric and magnetic fields of the electron beam and longitudinal magnetic field of the cooler:

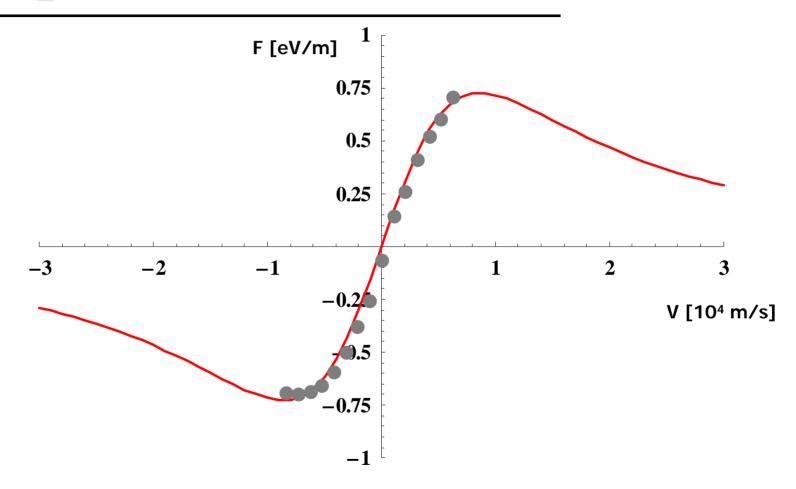
$$v_d = \frac{2I}{B\beta\gamma^2} \frac{r}{a^2}$$

For measured distribution of the proton beam for the case under comparison (March 2, set#23, B=0.1T, Ie=500mA) - V_drift=6-7*10^3m/s - which is an additional contribution to V_effective in the cooling force formulas.





March 2 data: Ie=500mA, B=0.1T - formula vs experiment with additional contribution to V_effective from V_drift







Fits with single-particle formulas

- 1. Current dependence friction force scales linearly with current/density as expected from formula.
- 2. Numeric coefficient for the force is in agreement with the one in Parkhomchuk's formula. Also, it can be adjusted to agree with Derbenev's coefficient (which results in only slightly different effective velocity) the coefficients are similar for the region of low relative velocities $(1/\pi \text{ vs } 1/(2\pi)^{1/2})$.
- 3. Note that Coulomb logarithm depends on relative ion velocity and V_effective fitting was done with such velocity-dependent logarithm.
- 4. Fitted V_effective has very weak current dependence: 0.74-0.78*10⁴ m/s





Observations

- Using single-particle formula allows to fit experimental data and extract V_effective.
- However, since rms velocity spreads of cooled proton beam are significant (for our measurements, we would need to have dp/p=1e-5 and ε =1e-9 m rad to neglect this effect, while parameter of the proton beam with which we did measurements typically had about dp/p=5e-5 and ε =5e-8 m rad), fitted V_effective has contribution from this effect.

The accurate procedure is then to measure rms velocities of the distribution and average single-particle formulas over the proton distribution.

This was done for all 10's of friction force curves which were measured for various parameters





Detailed comparison: Averaging over ion distribution

$$\langle F \rangle = C \frac{4\pi Z^{2} e^{4} n_{e}}{m\sqrt{2\pi} \Delta_{\perp}^{2} \Delta_{\parallel}} \int_{0}^{\infty} \int_{-\infty}^{\infty} \frac{v_{\parallel} L_{M}(v_{\perp}, v_{\parallel}, v_{eff})}{(v_{\perp}^{2} + v_{\parallel}^{2} + v_{eff}^{2})^{3/2}} \exp \left(-\frac{v_{\perp}^{2}}{2\Delta_{\perp}^{2}} - \frac{(v_{\parallel} - v_{0})^{2}}{2\Delta_{\parallel}^{2}}\right) v_{\perp} dv_{\parallel} dv_{\perp}$$

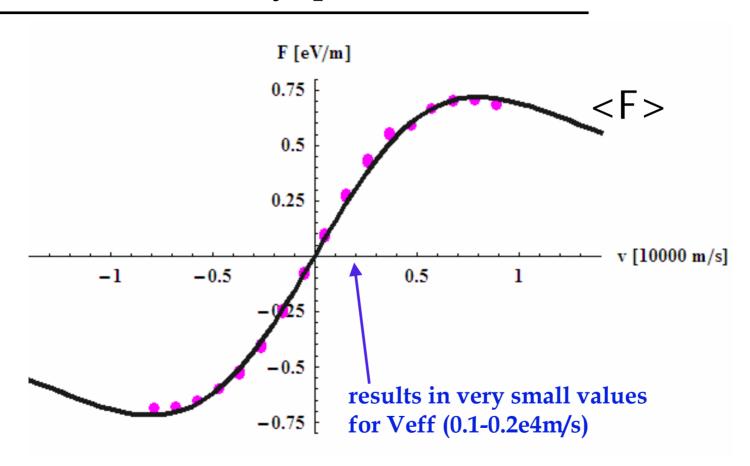
rms parameters of proton beam were measured for each measurement of friction force curve.

- 1. First approach: assume C is known and treat V_{eff} as fitting parameter.
- 2. Second approach: assume V_{eff} is known from measurements and treat C as fitting parameter.





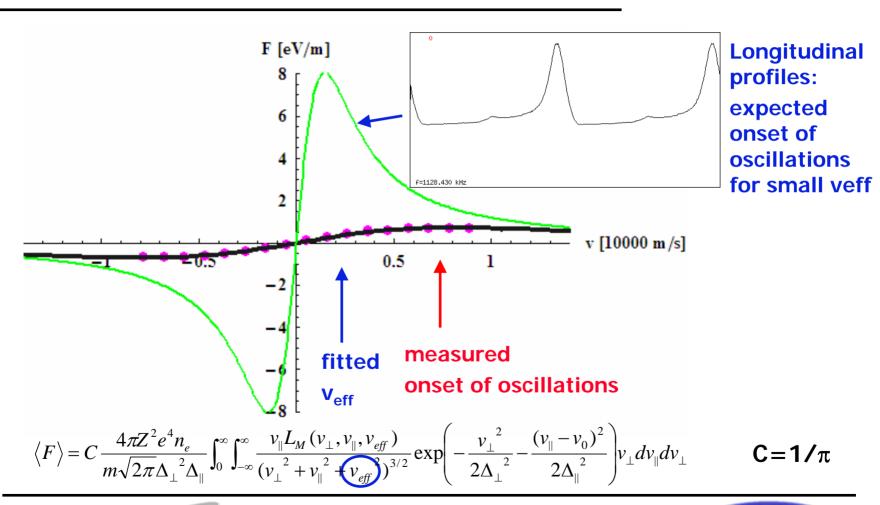
B=0.12T, Ie=300mA Friction force averaged over proton distribution with measured rms velocity spread







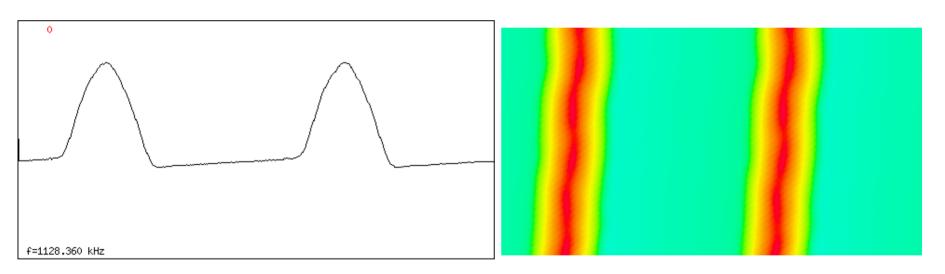
First approach – one fitting parameter Veff





Measurements of longitudinal friction force maximum

Approaching friction force maximum



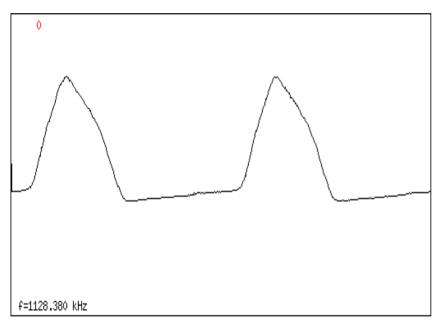
Longitudinal profiles

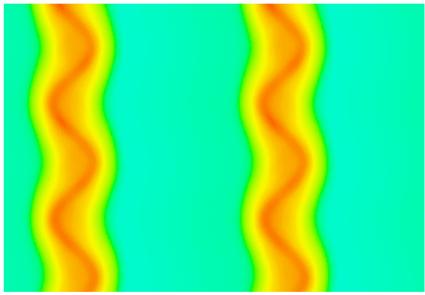




Measurements of longitudinal friction force maximum

just past the maximum



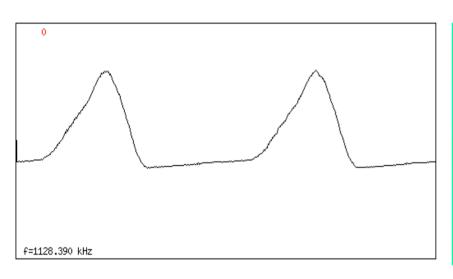


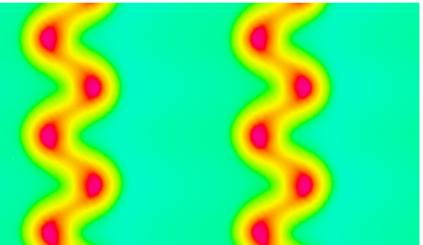




Measurements in non-linear part of the friction force

far past the maximum

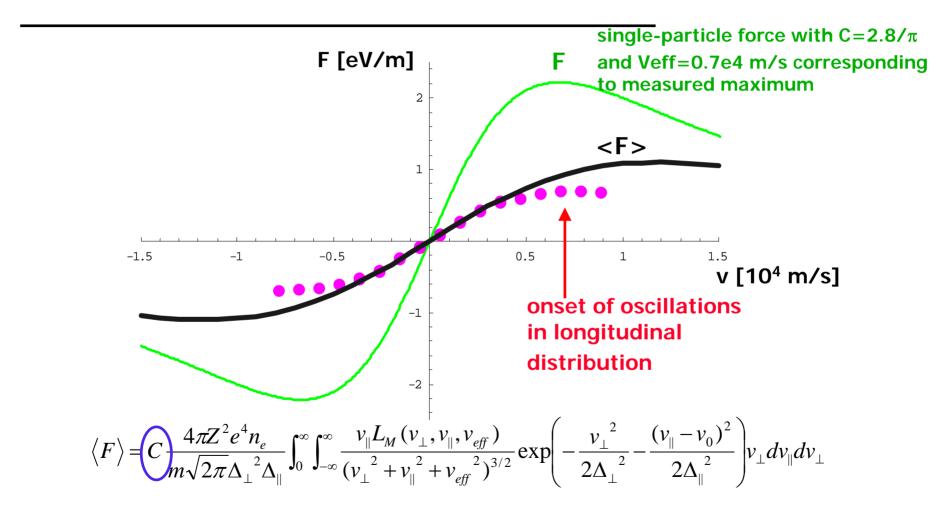








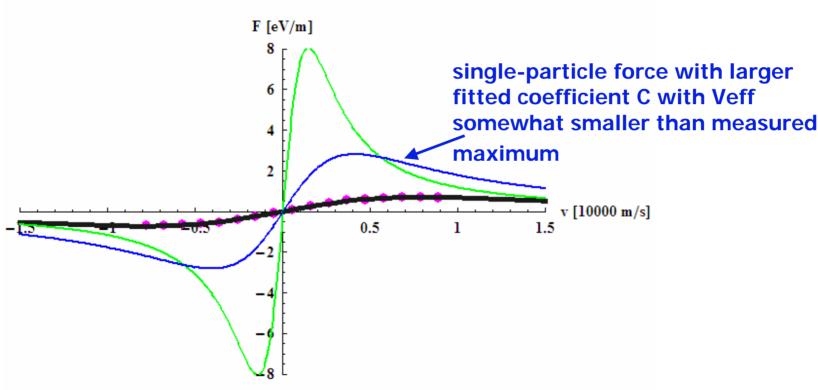
Second approach – one fitting parameter C (with measured Veff)







60



$$\left\langle F \right\rangle = \bigcirc \frac{4\pi Z^{2} e^{4} n_{e}}{m\sqrt{2\pi}\Delta_{\perp}^{2}\Delta_{\parallel}} \int_{0}^{\infty} \int_{-\infty}^{\infty} \frac{v_{\parallel} L_{M} \left(v_{\perp}, v_{\parallel}, v_{eff}\right)}{\left(v_{\perp}^{2} + v_{\parallel}^{2} + v_{eff}^{2}\right)^{3/2}} \exp \left(-\frac{v_{\perp}^{2}}{2\Delta_{\perp}^{2}} - \frac{\left(v_{\parallel} - v_{0}\right)^{2}}{2\Delta_{\parallel}^{2}}\right) v_{\perp} dv_{\parallel} dv_{\perp}$$





Summary - benchmarking of experiments

At CELSIUS, we were able to measure longitudinal friction force with very good precision which allows us to use experimental data for accurate benchmarking of theory and simulations.

Parameter dependence of the friction force was measured with "well controlled" condition:

- 1) Current dependence
- 2) Dependence of tilt between electron and proton beams
- 3) Dependence on solenoid errors
- 4) Various degrees of magnetization
- 5) Transient cooling

Benchmarking of experimental data for each of the experiments is presently in progress.





Acknowledgements

We would like to thank I. Ben-Zvi, V. Litvinenko, A. Burov, Ya. Derbenev and Electron Cooling Group of RHIC for many useful discussions and help during these studies.

Numerical studies became possible due to support and constant help of Tech-X Corp. with the VORPAL code and Dubna Cooling group with the BETACOOL code

Experimental studies became possible due to a strong interest expressed by the CELSIUS group. We thank Dag Reistad and The Svedberg Laboratory for providing beam time and support during these experiments. We also thank Oliver Boine-Frankenheim for taking an active role in planning of these experiments.





Thank you for your attention!

